

# “Investigations on the abrasivity of iron ore slurries : selection of materials for pipelines applications in mine industry”



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Co-workers: IC and Graduated Students



**LESTA**

LABORATÓRIO DE ENGENHARIA  
DE SUPERFÍCIES E TÉCNICAS AFINS

*Summary:*

- . Introduction to the ASTM standard method: procedures, equipment, data acquisition and treatment.*
- . Miller Index and SAR Number Machine: project and development*
  - . Case studies: results and discussion*
  - . Conclusions*



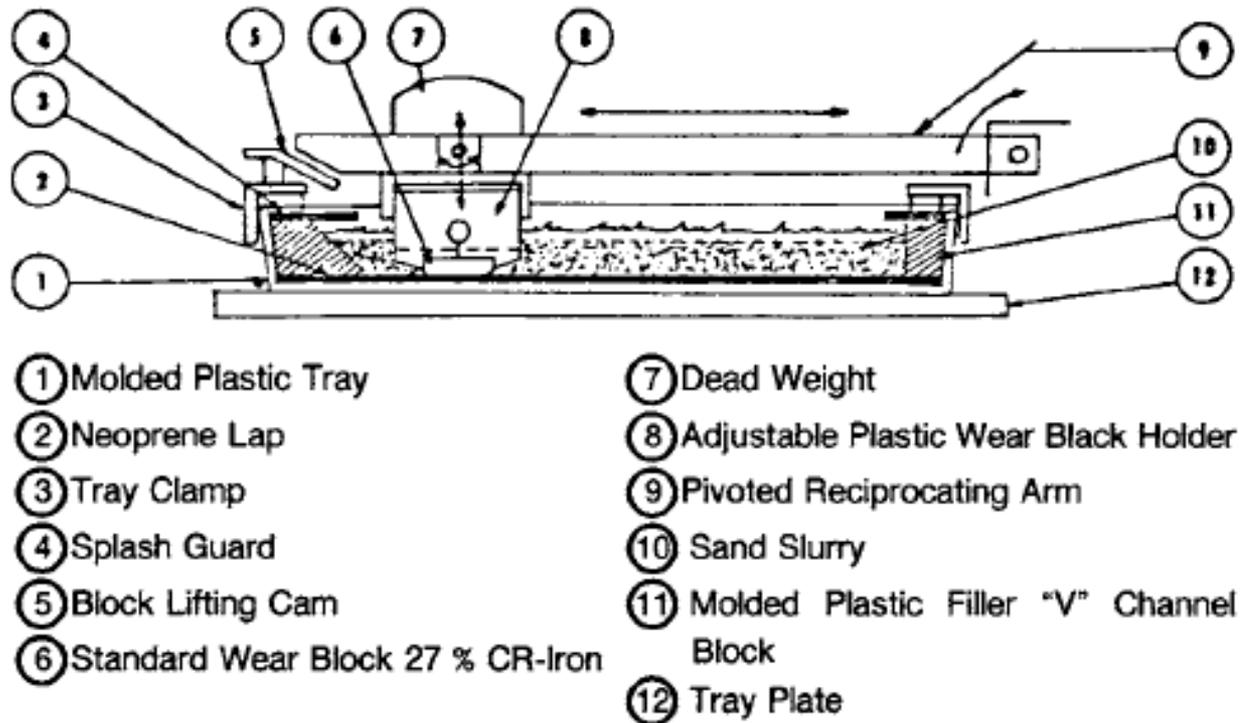
Standard ASTM G75-07

**STANDARD TEST METHOD FOR  
DETERMINATION OF SLURRY ABRASIVITY  
(MILLER NUMBER) AND SLURRY ABRASION  
RESPONSE OF MATERIALS (SAR)**

## Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials

- Determining the relative abrasivity of any slurry (Miller Number) or the response of different materials to the abrasivity of different slurries (SAR Number).
- "Number Miller" slurry is a measure of the abrasiveness related to the mass loss rate of a standard metal block.
- "SAR number" is a measure of the relative abrasion response of any material in any slurry.

# Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials



Miller Number Machine Slurry: Cross-Section.



Neoprene lap after abrasion test

# Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials

The nominal composition of the chromium-iron wear block reference material is: Carbon-2.5 %, Manganese-1.0 %, Silice-0.6 %, Nickel-0.25 %, **Chromium-28 %**, Molybdenum-0.3 %, Vanadium-0.8 %.

6-h test, run in 2-h increments.

# Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials

## Procedure

Wear Specimen Preparation;

Slurry Preparation;

Filling Slurry Troughs;

Start the test for 2 hours;

Stop and remove the wear blocks;

Clean and weigh each wear block;

Alternating the orientation of the wear blocks for each of the three 2-h.

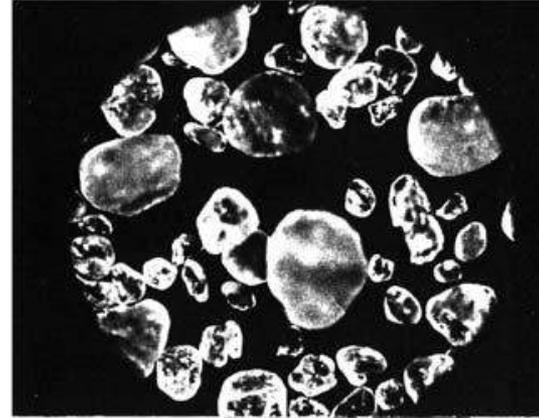
Remix any settled slurry in each trough before each 2-h run.;

Record the wear block mass loss for each run.

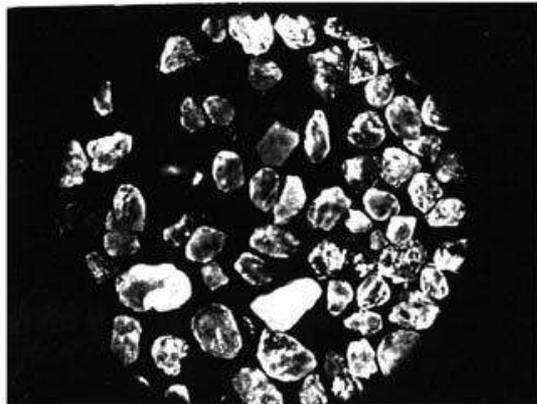
Selected abrasive particles and their correspondent Miller Number.



Bunker Hill Sand  
Miller Number 218



Saskatchewan Sand  
Miller Number 149



Los Angeles Sewer Sludge  
Miller Number 77



AFS 50-70 Test Sand  
Miller Number 136

# Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials

Results:

**TABLE 1 Test Data**

Wear Specimen	142		143	
	Mass, g	Cumulative Loss, mg	Mass, g	Cumulative Loss, mg
Initial	16.2810	0.0	16.2670	0.0
After 2 h	16.2723	8.7	16.2580	9.0
After 4 h	16.2668	14.2	16.2500	17.0
After 6 h	16.2594	21.7	16.2406	26.4

$$MN = (18.18 \text{ h/mg}) \times (\text{mass loss rate, mg/h})$$

$$\text{SAR Number} = \text{Miller Number} \times (7.58/\text{SG specimen})$$

# Standard Test Method for Determination of Slurry Abrasivity (Miller Number) and Slurry Abrasion Response of Materials

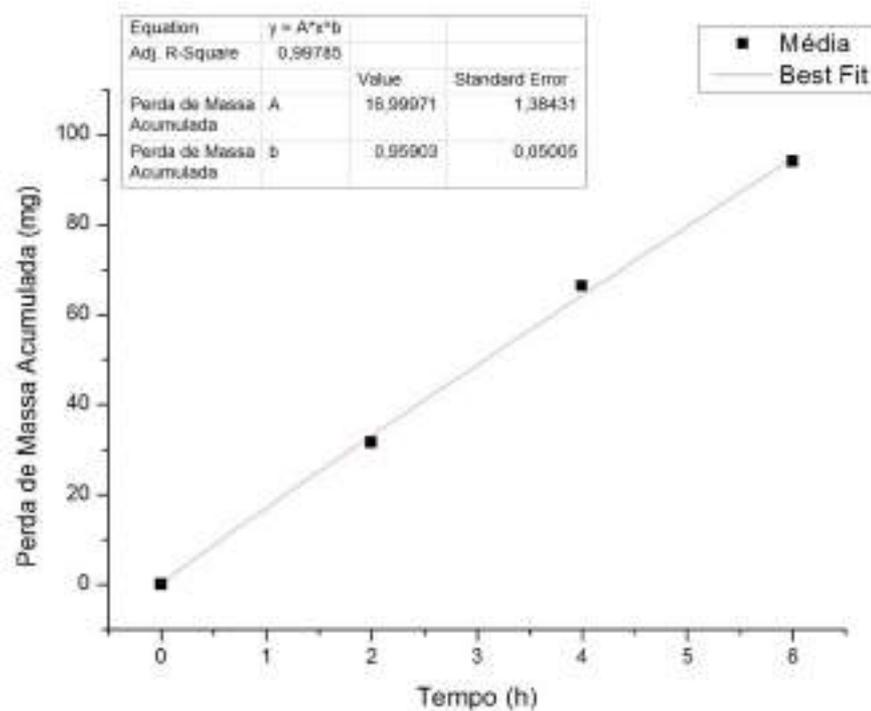
NOTE 1—Generic minerals from different sources differ greatly in abrasivity.

Material	Miller Numbers
Alundum 400 mesh	241
Alundum 200 mesh	1058
Ash (fly)	83, 14
Bauxite	9, 22, 33, 45, 50, 76, 134
Clay	34, 36
Coal	6, 7, 9, 10, 12, 21, 28, 47, 57
Copper concentration	19, 37, 58, 68, 111, 128
Gypsum	41
Iron Ore	28, 37, 64, 79, 122, 157, 234
Kaolin	7, 7, 30
Lignite	14
Limestone	22, 27, 29, 30, 33, 39, 43, 46
Limonite	113
Magnetite	64, 67, 71, 134
Mud, drilling	10
Phosphate	68, 74, 84, 134
Potash	0, 10, 11
Pyrite	194
Sand/sand fill	51, 59, 75, 85, 93, 116, 138, 149, 246
Shale	53, 59
Sewage (raw)	25
Sulfur	1
Tailings (all types)	24, 61, 76, 91, 159, 217, 480, 644

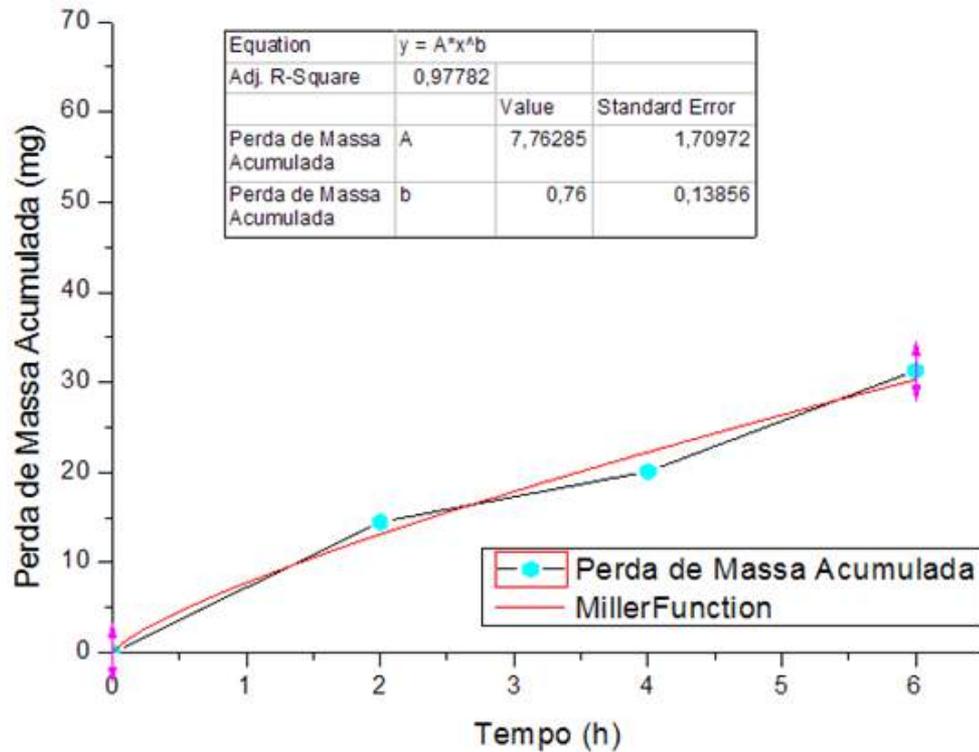
Examples of Miller Numbers for Some Slurries

# *How to achieve abrasivity coefficients: time dependence of mass loss*

$$y = A \cdot x^B$$



## Typical graph relating loss mass x time



## Miller-Number

The Miller-Number (MN) describes the abrasivity of any slurry. It is used to rank the abrasivity of slurries in dependency of the wear of a standard reference material . The higher the Miller Number, the higher the wear damage on the reference block. It is related to the mass loss rate of a standard wear specimen two hours into an abrasive test. These tests add up to a curve in the cumulative “mass loss x time” diagram. The curve can be approximated with the potential function shown in Equation 1.

$$M(t) = A \cdot t^B \quad (1)$$

Exponential function to approximate the Miller-Test curve with:

$M(t)$  = cumulative mass loss in mg,

A = first curve fit coefficient,

B = second curve fit coefficient and

t = time in h

The mass loss rate after two hours is the slope at this point of the calculated curve. The slope is the y-value of the derivation of Equation with an x-value of two. The derivation is shown in the following Equation 2.

$$M'(t) = A \cdot B \cdot t^{(B-1)} \quad (2)$$

Equation: Derivation of Equation 1:

$M'(t)$  = mass loss rate in mg/h

A = first curve fit coefficient,

B = second curve fit coefficient and

t = time in h (for MN calculation 2)

To get a significant number to express the abrasion effects, a scaling factor  $C = 18,18 \text{ mg/h}$  is used, which leads to Equation 3. The result is rounded to the next integer. Values will be approximately 1 for slurry of sulphur with 50% diluted and 1000 for 220-mesh slurry of Corundum also 50% water diluted.

$$MN = C \cdot M' \quad (3)$$

Equation 3: Calculation of the Miller-Number with

MN = Miller-Number

C = scaling factor (18,18 mg/h)

$M'$  = mass loss rate in mg/h

### **Slurry Abrasivity Response Number**

The Slurry Abrasivity Response Number (SAR-Number) is the relative abrasive response of any material in any slurry. It is generalized from the Miller Number and is not bound to the standard reference material. The SAR-Number is usually used **to rank construction materials of fluid handling equipment for special slurry**. The higher the SAR Number the poorer is the material resistance against wear.

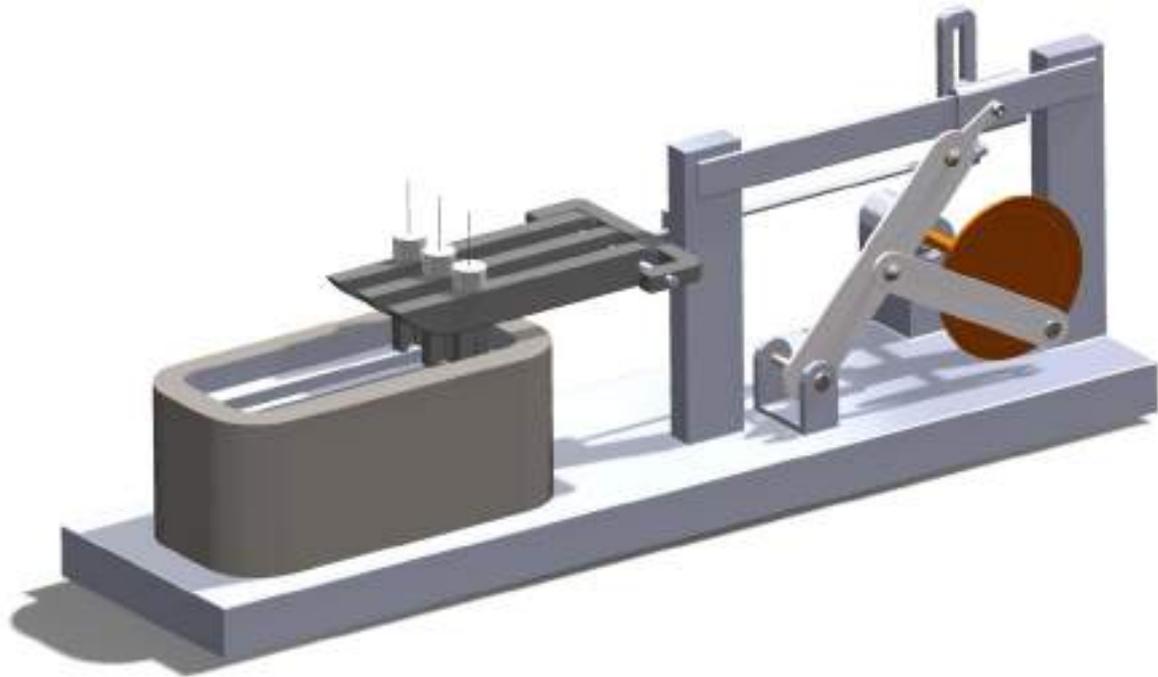
# Abrasion Test Machine: Project



Explodida.avi

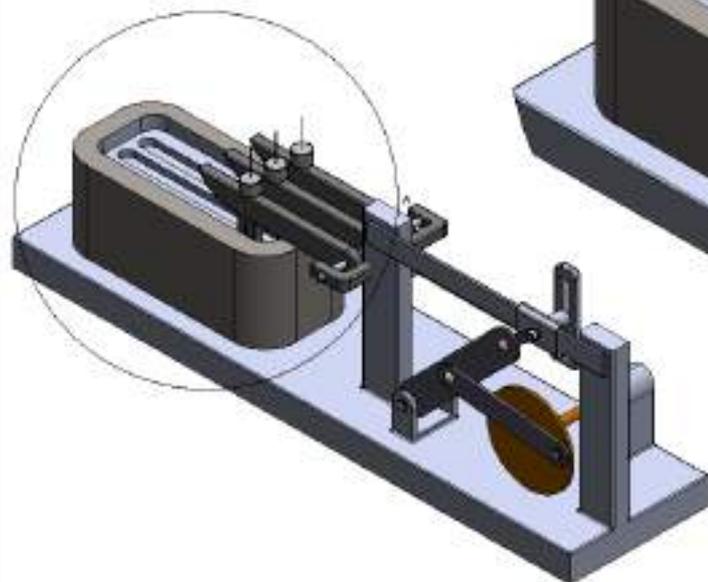


MontagemFinal 2.avi



## SAR Machine

PROJETO LESTA - 2015  
COLABORAÇÃO: Francisco Siqueira & Ricardo da Rocha  
Equipamento para realização de ensaio abrasivo de papéis minerais  
PROFESSOR ORIENTADOR: Adilson Rodrigues da Costa  
Todos os direitos reservados

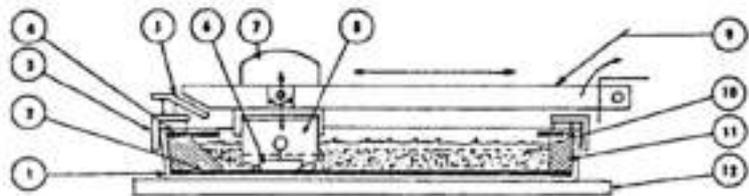


DETALHE A  
ESCALA 1:1

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<b>LESTA</b>	LABORATÓRIO DE ENGENHARIA DE SISTEMAS E TÉCNICAS AVANÇADAS
Montagem Versão 2	
www.IGRETA.FE.UEFOP.BR	
<b>SAR Machine</b>	AD
BRUNOPIRE	BRUNOPIRE

# Methodology

## Miller Machine



- ① Molded Plastic Tray
- ② Neoprene Lap
- ③ Tray Clamp
- ④ Splash Guard
- ⑤ Block Lifting Cam
- ⑥ Standard Wear Block 27 % CR-Iron
- ⑦ Dead Weight
- ⑧ Adjustable Plastic Wear Block Holder
- ⑨ Pivoted Reciprocating Arm
- ⑩ Sand Slurry
- ⑪ Molded Plastic Filler "V" Channel Block
- ⑫ Tray Plate



## Chart of mass loss data

Time (h)	Specimen 1		Specimen 2		Specimen 3	
	Mass (g)	Mass loss (g)	Mass (g)	Mass loss (g)	Mass (g)	Mass loss (g)
0	0,0000	0,0000	1,6472	0,0000	1,5952	0,0000
2	0,0000	0,0000	1,6288	0,0184	1,5846	0,0106
4	0,0000	0,0000	1,6263	0,0025	1,5758	0,0088
6	0,0000	0,0000	1,6080	0,0183	1,5717	0,0041
	Accumulated mean mass loss Média					
	(g)	(mg)				
	0,0000	0,0				
	0,0145	14,5				
	0,0201	20,1				
	0,0313	31,3				

# Case studies

## **I - Investigation on the abrasivity of mining slurries in respect to the properties of the abrasive particles: concentration and grain size. Part I**

- Frieder Kälber<sup>1</sup>; Steffen Meinhold<sup>1</sup>; Francismar Siqueira<sup>2</sup> ; Paulo Ricardo <sup>3</sup>; A. R. da Costa<sup>4</sup>

1 – Reutlingen University – Germany

2,3 e 4: OP School of Mines

# Slurries abrasivity tests

## Slurry: Iron ore (Run Of Mine – Milled)

Room temperature in the Laboratory:  $25^{\circ}\text{C} \pm 1^{\circ}\text{C}$

Relative Humidity in the Laboratory: 75%

## Wear specimen :

Material: API X70 Steel

Density:  $7,8\text{g}/\text{cm}^3$

Specimen	HV 0,01 [N/mm <sup>2</sup> ] Ferrite	HV 0,05 [N/mm <sup>2</sup> ] Perlite
API X70	173,8	278,8

Results of the micro hardness tests on the wear specimen

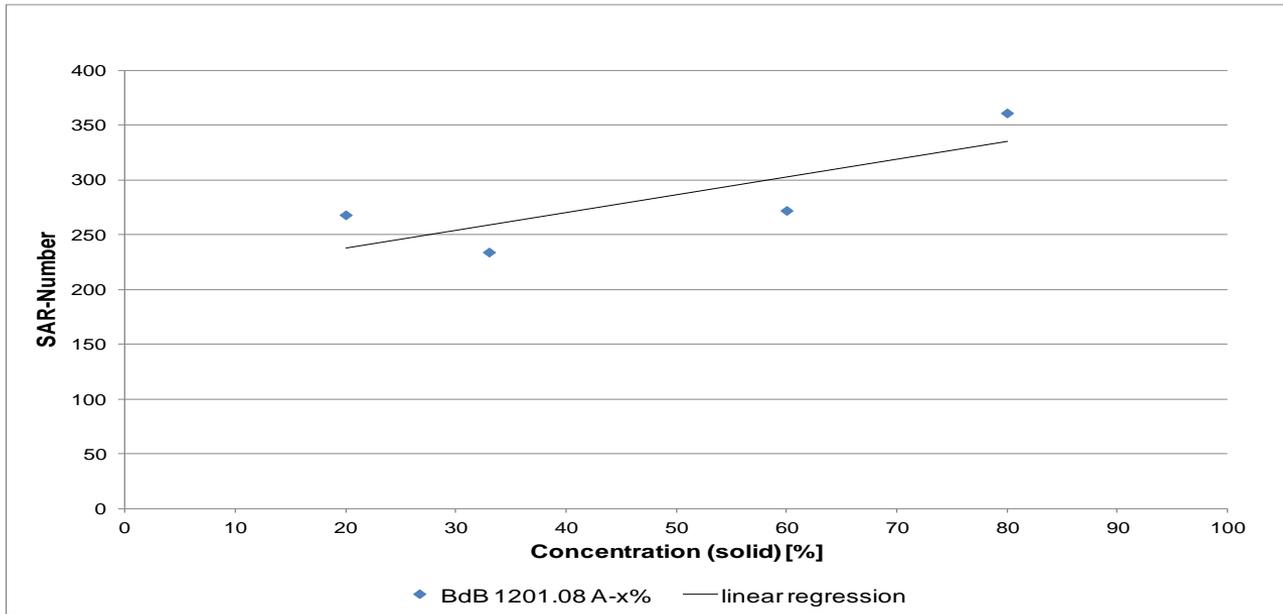
## Pad material:

Descrição: Neoprene

Hardness "Shore A": 75

Elastic Constant (k) =  $930\text{ N}\cdot\text{m}^{-1}$





Evolution of SAR-Number with different concentration (dilution)(slurry A (x%))

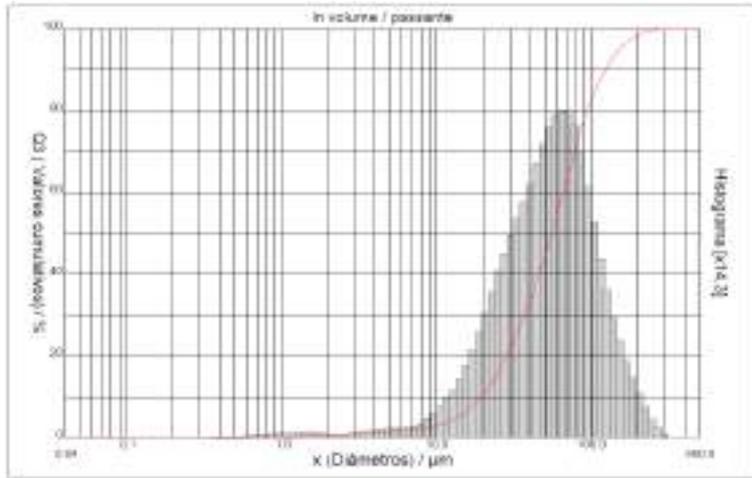
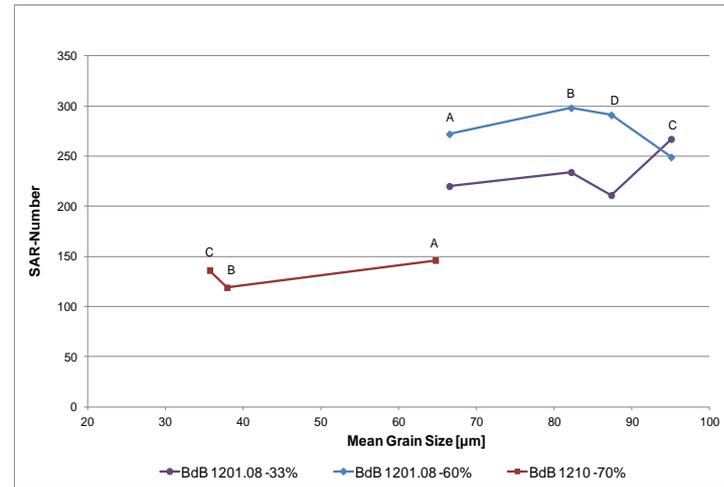


Diagram of grain size analysis of the slurry BdB 1210 A



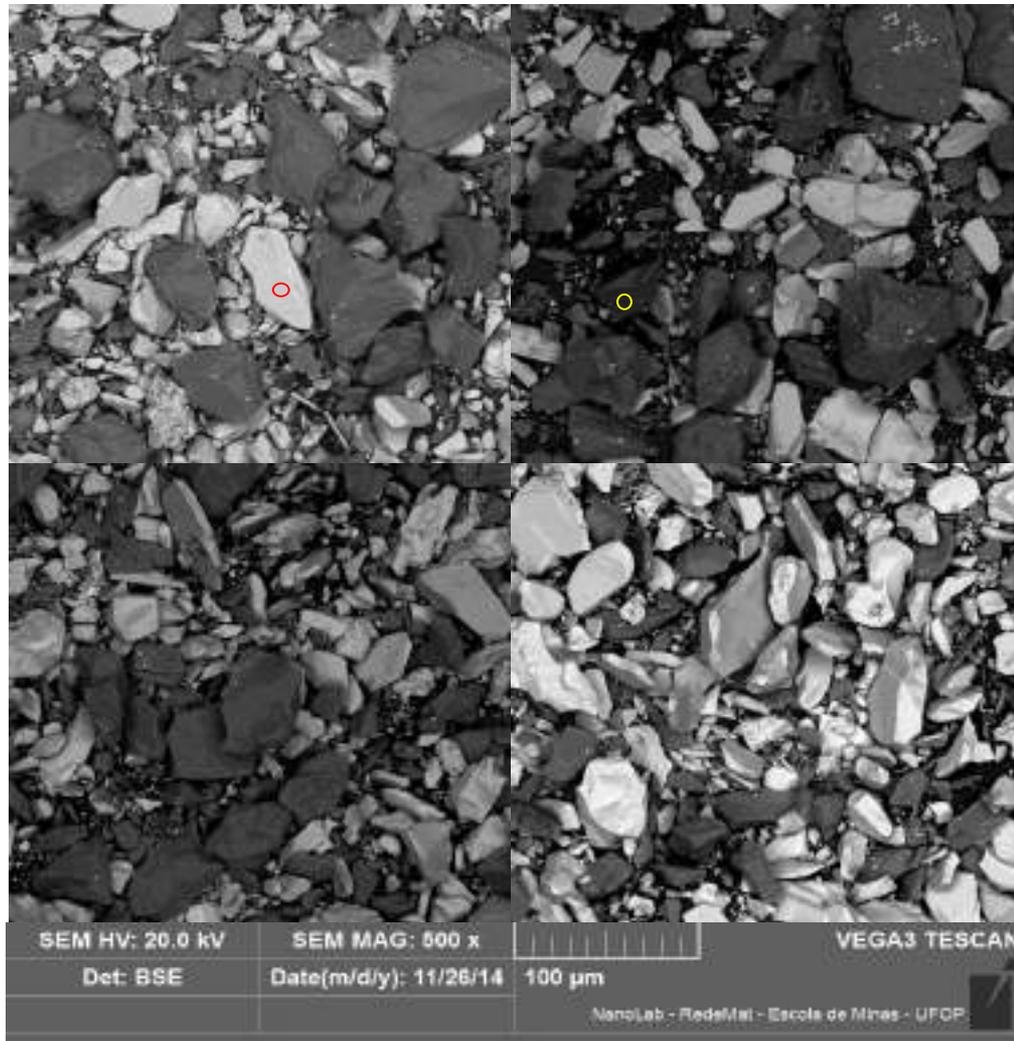
Mean grain size and related SAR-Numbers of the different batches

# **II - Investigation on the abrasivity of mining slurries in respect to the properties of the abrasive particles: morphology, hardness and nature of particles. Part II**

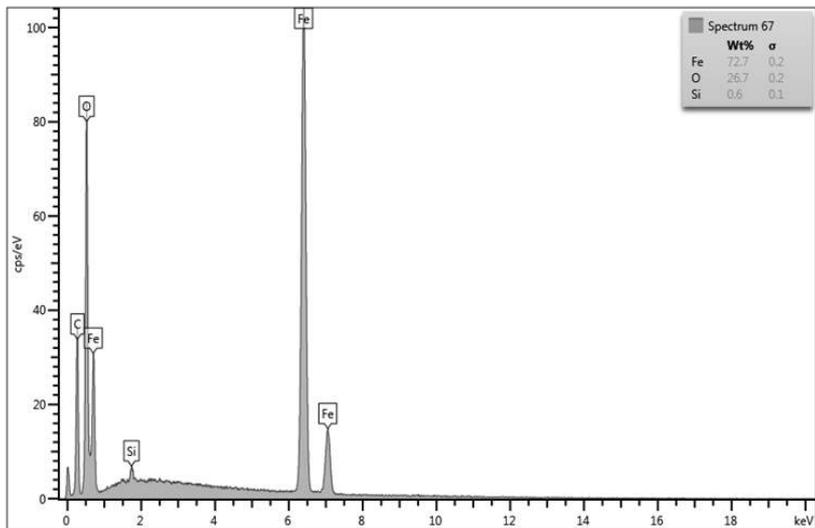
Frieder Kalber<sup>1</sup>; Steffen Meinhold<sup>1</sup>; Francismar Siqueira<sup>2</sup>; Paulo Ricardo<sup>3</sup>; A. R. da Costa<sup>4</sup>

1 – Reutlingen University – Germany

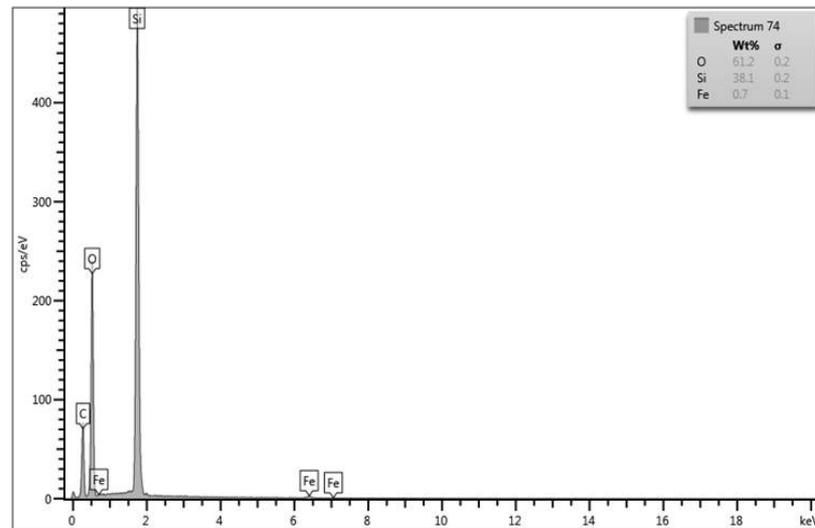
2,3 e 4: OP School of Mines



Microscopic recording of the particles of the slurries from the batch BdB 1201.08 in BSE mode: Top left: A/Top right: B/Bottom left: C/Bottom right: D



EDS diagram for bright particles (Hematite)



EDS diagram for dark particles (Silica)

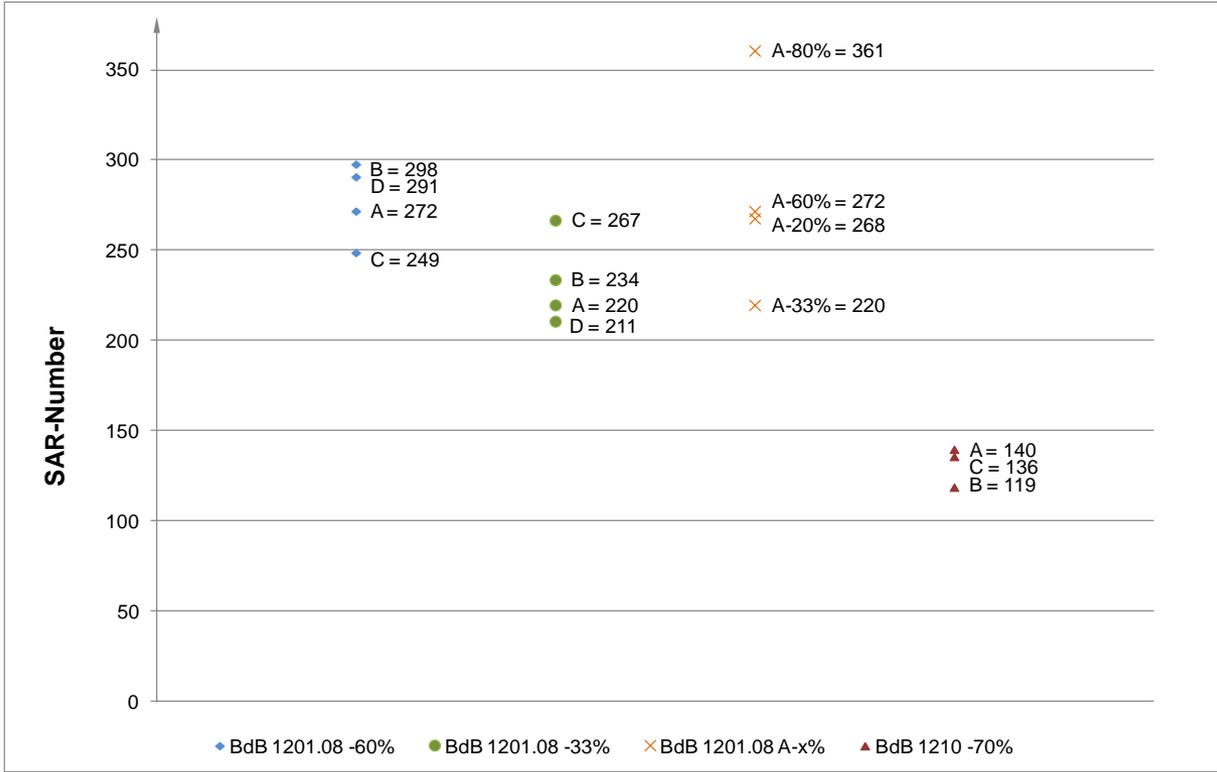
Hardness of Hematite is around 650 HV and for Silica this property may attain 1000 HV.

Slurry	BdB 1201.08 A	BdB 1201.08 B	BdB 1201.08 C	BdB 1201.08 D
Proportion hematite [%]	60	50	60	80
Proportion silica [%]	40	50	40	20

Ratio of hematite and silica in the slurries from batch BdB 1201.08

Name of sample slurry	Cumulative mass loss [mg/h]	MN-Number	SAR-Number
BdB 1201.08 A -20%	16,50	276	268
BdB 1201.08 A -33%	13,26	226	220
BdB 1201.08 A -60%	15,39	280	272
BdB 1201.08 A -80%	20,44	372	361

MN and SAR Number of the Slurry BdB 1201.08 A -x% with different



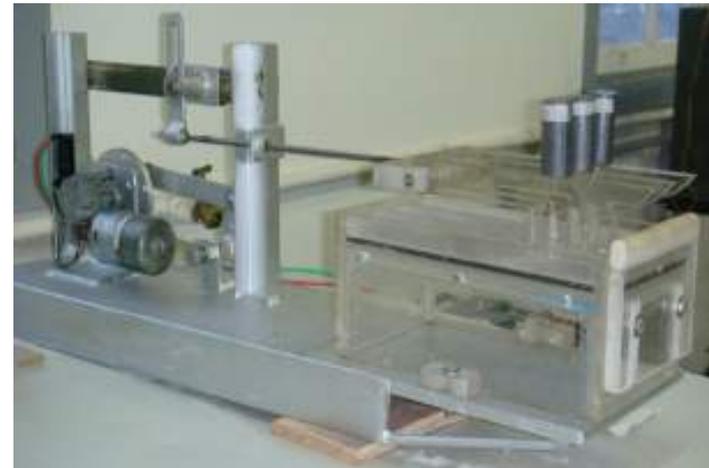
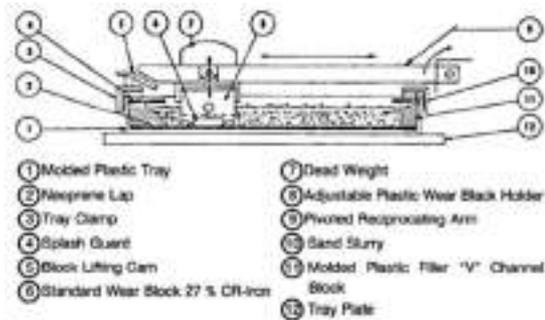
Name of sample slurry	mean diameter [ $\mu\text{m}$ ]
BdB 1201.08 A	66,54
BdB 1201.08 B	82,2
BdB 1201.08 C	95,06
BdB 1201.08 D	87,36
BdB 1210 A	64,77

Mean grain size

The morphology of the particles is analysed based on the BSE pictures from the SEM. Previous figure shows the pictures of the slurries BdB 1201.08 A,B C and D. In these slurries the particles look similar. The silica particles are big polyhedral bodies with a rough surface. The edges have mostly obtuse angles. This makes it possible for the particles to act as a rolling element. The hematite is mostly present in small fractures but also in greater particles. On the larger particles great planes can be seen, which is due to the hexagonal crystal system. In this case the particles are present as “Tabular Plates”. With these parallel lying surfaces the particles look like plates. The angles of the edges are likely acute. In contrast to the silica particles, these would likely perform sliding movements.

# Abrasion wear of polyurethane

## III - Wear of Polyurethane under slurry abrasivity test



## Polymers in mine industry

### Why Polyurethane?

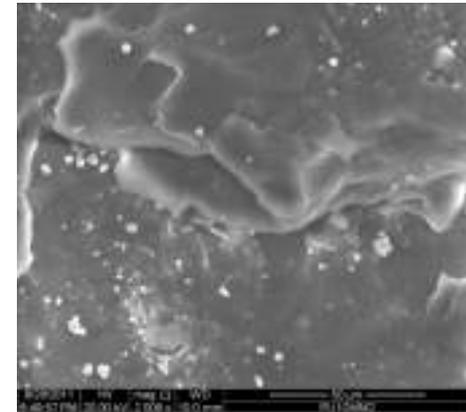
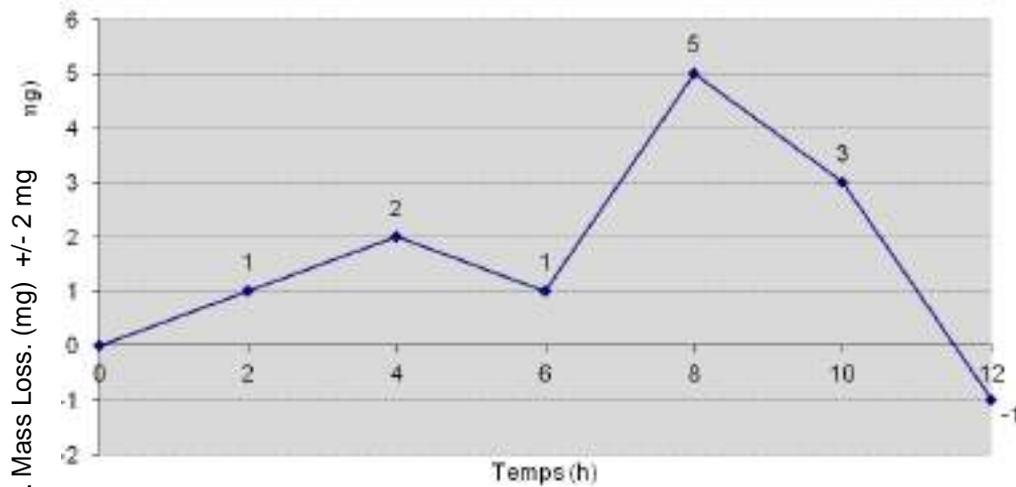


	<b>« Adapted » Miller ASTM G75</b>
Slurry	SiO <sub>2</sub> (Sílica) + Fe <sub>3</sub> O <sub>2</sub> Hematite 50% de sólidos + Distiled Water Room Temperature : 18°C +/- 2°C
Sample	Polyurethane Density : 1,1 g/cm <sup>3</sup> Hardness : 90 Shore A
Pad	Glass Hardness : 6 Mohs

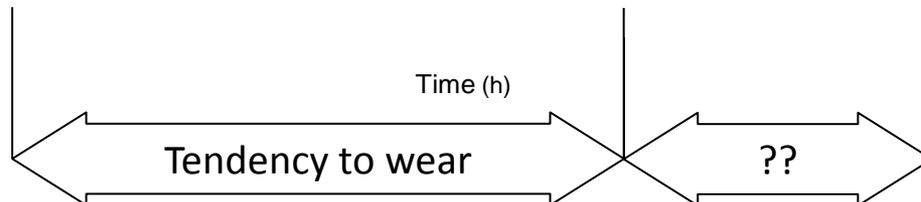
# Test 1

## Parameters

Load	15 g – 0,3 g/mm <sup>2</sup>



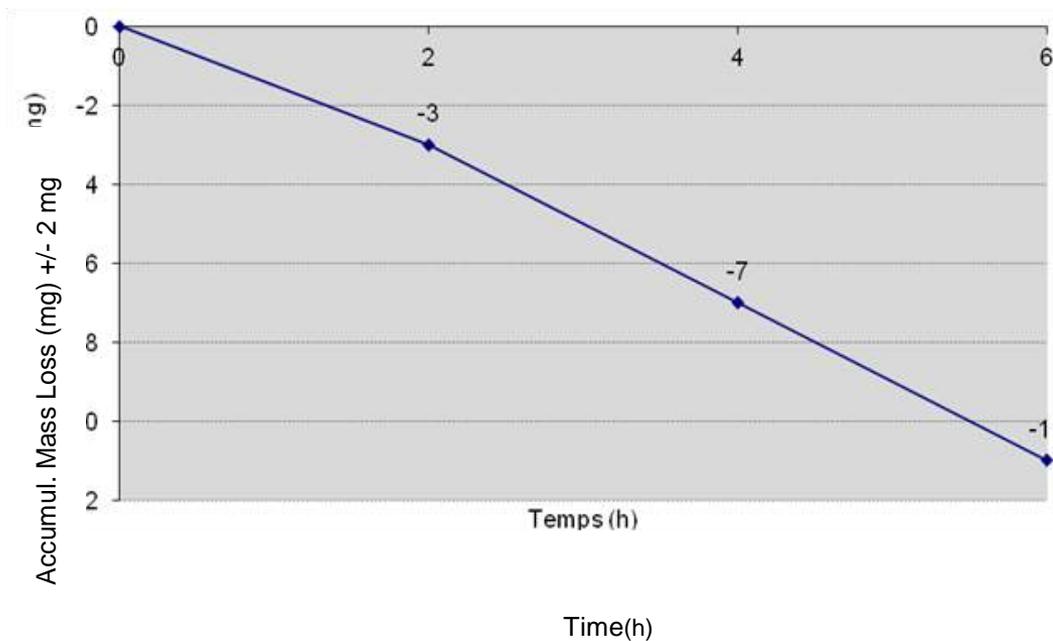
SEM – Embedded abrasive particles



# Test 2

## Parameters

Load	50 g – 1 g/mm <sup>2</sup>

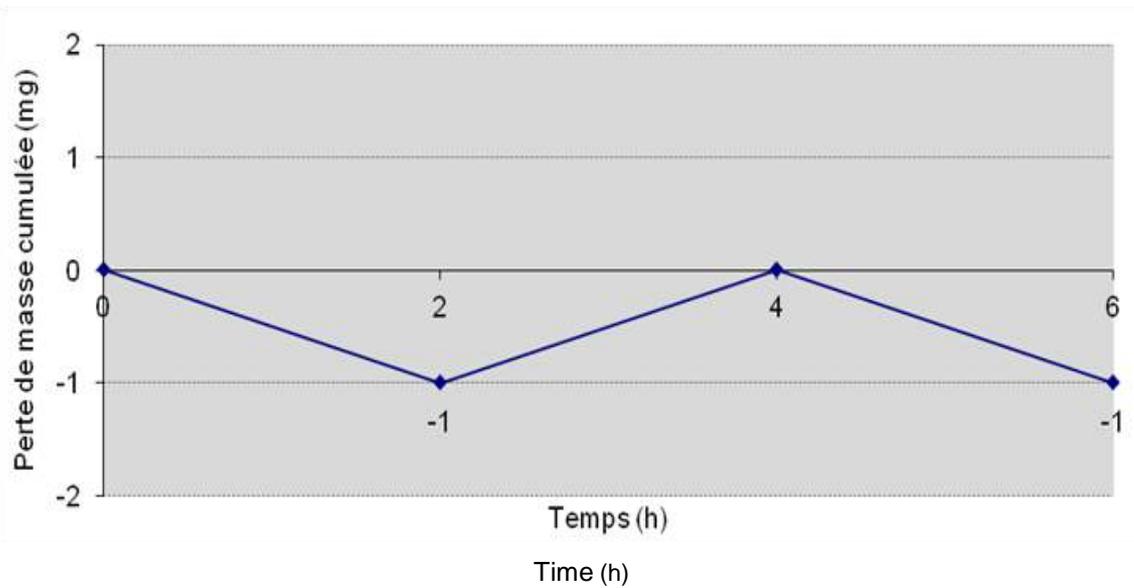


- Particle Adhesion
- Role of the applied charge (Load)

# Test 3

## Parameters

Load	0 g/mm <sup>2</sup>

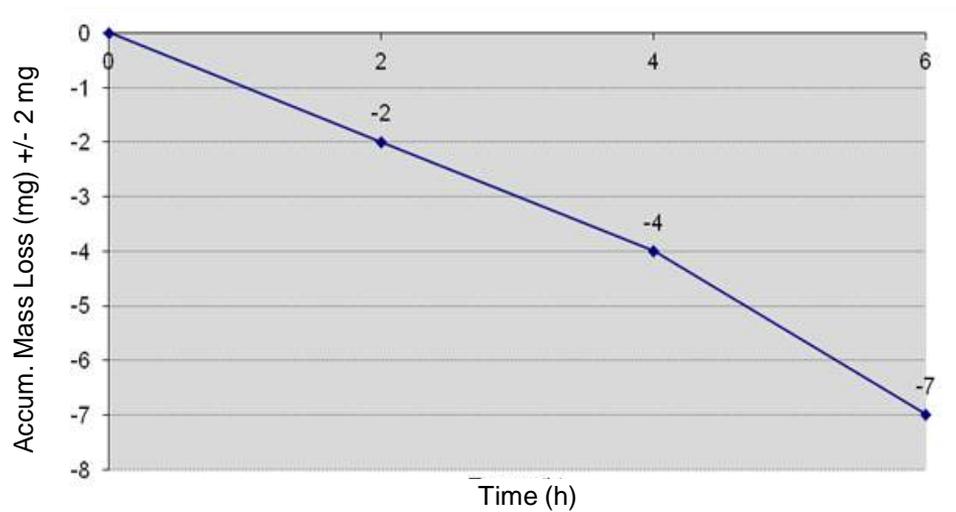


→ Values have no significance

# Test 4

## Parameters

Load	93 g – 2,0 g/mm <sup>2</sup>



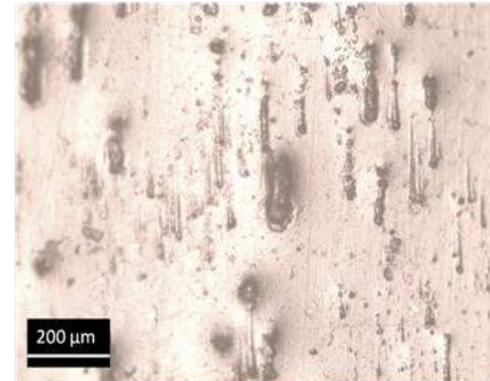
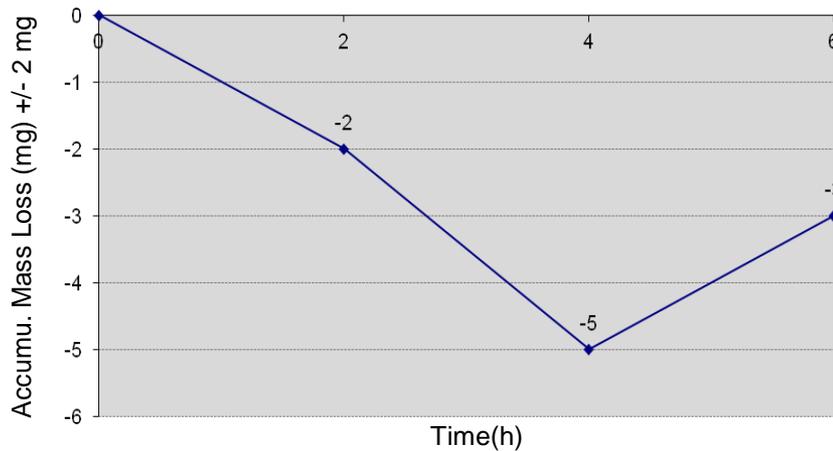
- Significant values
- Increased particle adhesion

# Test 5

Parameters (the same as in Test 1)

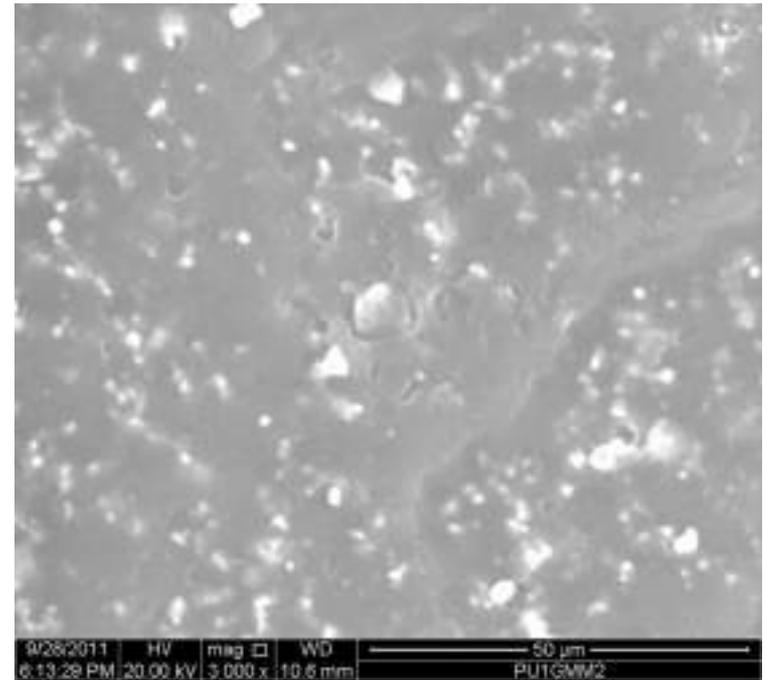
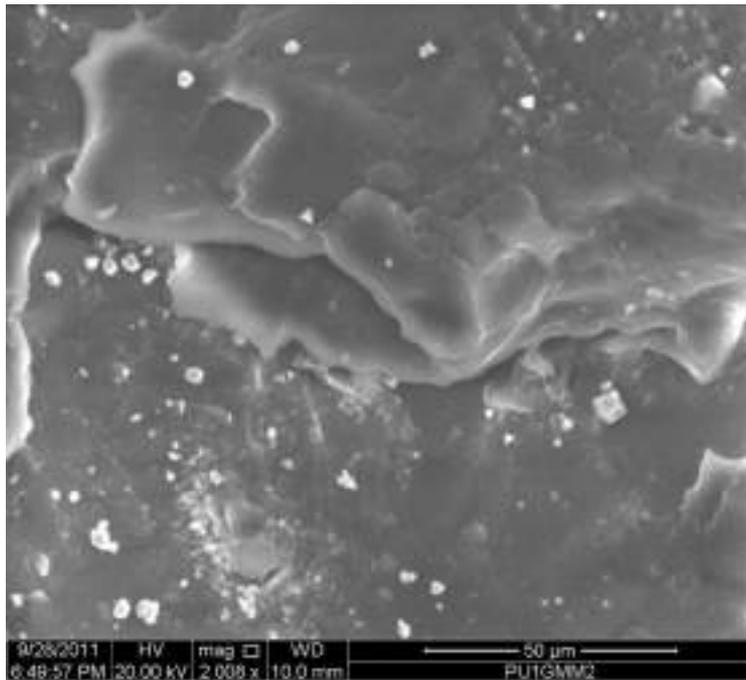
Load	15 g – 0,3 g/mm <sup>2</sup>

→ Previous Roughness influencing behaviour  
(fatigue, adhesion)



Irregularities in sample surface

# Abrasive particles embedded in polyurethane and fatigue cracks



# Conclusions

- Abrasion tests based on Miller`s procedures allow understand many aspects of wear phenomena and correlate them to microstructure of materials.
- Materials may be ranking accordingly to their response to the abrasivity of the slurries allowing better decision in selection of materials for engineering projects.
- Some procedures proposed in ASTM G75-07 standard need to be changed or redefined, otherwise the test can not be adopted as a “standard”.

# Bibliography

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Thank you all!

